

Packaging materials with a foam layer of for example
10 polypropylene in the form of virtually continuous, reeled
webs are used for the production of thermoformed, self-
supporting packages such as for example trays for packaging
foodstuffs. To this end, such packaging materials may be
converted into packages on "FFS machines" (form-fill-seal
15 machines), wherein the packaging material in web form is
fed into a forming apparatus, is shaped therein into a web
of trays, the material to be packaged is introduced into
the trays, which are closed by heat-sealing with a
preferably transparent film. The closed trays may then be
20 separated from one another.

30

Packaging materials comprising a layer of foamed polypropylene for the production of packaging trays by

- 2 -

thermoforming are described for example in EP-A-0 570 222. These materials comprise a foam layer and a multilayer composite film, which may optionally contain a barrier layer which makes the packaging material gas- and aroma-
5 tight. This multilayer packaging material does not always exhibit the desired properties for self-supporting packages.

EP-B-1 117 526 discloses complementing the foam layer with
10 a compact layer of a polyolefin of the foam layer while maintaining a specific thickness ratio of these two layers to one another in order to improve the self-supporting properties of packages produced from this packaging material without increasing the thickness of the packaging
15 material.

Although this packaging material may very readily be converted into packages, for example by thermoforming, there is a requirement due to ever higher packaging
20 machinery running speeds to improve the packaging material in such a manner that it permits higher production speeds, i.e. shorter cycle times, without, for example, irregularities in the wall thickness of the packaging container consequently arising and without the mechanical
25 strength or rigidity and thus the self-supporting properties of the packaging container being impaired.

Said object is achieved according to the invention by providing a multilayered film which comprises the following
30 sequence of layers:

- 3 -

- A) a base layer of polyolefin foam containing 0.5 to 25 wt.%, relative to the total weight of the base layer, of at least one nucleating agent,
- B) a layer based on at least one polyolefin of the foam layer A),
- 5 C) optionally a bonding layer based on a polyolefin, which is preferably based on the particular monomer which is the main monomer of the polyolefin of foam layer A),
- 10 D) optionally a coupling agent layer,
- E) optionally a gas- and/or aroma-barrier layer,
- F) a coupling agent layer,
- G) an optionally heat-sealable and/or peelable surface layer,

15

wherein the total thickness of layers A) and B) is in the range from 0.5 to 2 mm and the thickness of layer B) is in the range from $\frac{1}{6}$ to $\frac{1}{2}$ of the thickness of layer A).

- 20 The total thickness of layers A) and B) is preferably in the range from 0.6 to 1.4 mm and the thickness of layer B) is in the range from $\frac{1}{6}$ to $\frac{1}{3}$ of the thickness of layer A).

- 25 The foam layer A) consists of at least one foamed polyolefin. Foamed propylene homo- and/or copolymers are here particularly suitable for the production of packages, such as for example packaging trays for packaging foodstuffs, as these materials exhibit self-supporting
- 30 properties even when they are of low thickness and low density. It is also possible to use blends of polyolefins to produce the foam layer. A blend of polypropylene having

long-chain branching and thus elevated melt strength and a propylene-ethylene copolymer, such as for example a heterophase propylene-ethylene block copolymer is in particular suitable. In particular, a blend of a
5 polypropylene with long-chain branching and a melt flow index (MFI) in the range from 1.4 to 4.2 g/10 min (2.16 kg, 230°C measured according to ISO 1133) and a heterophase propylene-ethylene block copolymer in a mixing ratio of 1:1 is suitable.

10

Foaming of the polyolefin of layer A) may proceed by the addition of solid, liquid and/or gaseous blowing agents, which are added to the polyolefin in conventional quantities, preferably in an amount of 0.5 to 3 wt.%.
15 Reference is here made to the disclosure in EP-A-0 570 222, which is hereby introduced as a reference and deemed to be part of the present disclosure.

The foam layer A) contains 0.5 to 25 wt.%, preferably 2.1
20 to 20 wt.%, particularly preferably more than 2.5 to 15 wt.%, relative to the total weight the foam layer A), of at least one nucleating agent. The nucleating agent is preferably finely divided with an average particle size in the range from 4 to 20 μm .

25

Suitable nucleating agents are any known solid nucleating agents, preferably synthetic or natural inorganic compounds. At least one nucleating agent selected from among the group comprising talcum, titanium dioxide,
30 silicon dioxide, calcium carbonate, magnesium silicate, aluminium silicate, calcium phosphate and montmorillonite

- 5 -

is particularly preferably used. Talcum is very particularly preferably used.

The nucleating agent is added to the polymer from which the
5 foam layer is to be produced, preferably in the form of a masterbatch which contains 30 to 60 wt.% of nucleating agent in the polymer, and is largely homogeneously dispersed therein prior to foaming.

10 The foam layer A) obtained therefrom are distinguished by an elevated number of cells with relatively small size deviations. The cell count is preferably greater than or equal to 250 cells/mm³, particularly preferably greater than or equal to 300 cells/mm³ up to 600 cells/mm³, the size
15 variations of the cells being in the range of $\pm 15\%$, preferably $\pm 10\%$. The density of the foam layer A) is preferably in the range from 0.35 to 0.55 g/cm³.

The density and cell count may moreover be varied by
20 process parameters, such as for example extrusion temperature or other process parameters, during the preferred production of the foam layer by extrusion and expansion.

25 Layer B) of compact polyolefin is substantially based on at least one polyolefin of the foamed base layer A). If this base layer consists of foamed polypropylene or a foamed blend of polypropylene and propylene-ethylene copolymer, the compact polyolefin layer B) is preferably based on
30 polypropylene or a propylene-ethylene copolymer. A heterophase propylene-ethylene block copolymer is particularly preferred. The melt flow index (MFI) of the

- 6 -

polyolefins used to produce layer B) is preferably in the range from 1.8 to 5.5 g/10 min measured as stated above. The thickness of layer B) amounts to $\frac{1}{6}$ to $\frac{1}{2}$, particularly preferably to $\frac{1}{6}$ to $\frac{1}{3}$ of the thickness of layer A).

Layer C) is preferably present, if layers D) to G) are prefabricated by coextrusion, preferably by blown film coextrusion, and are to be bonded with the other layers.

Layer C) is based on a polyolefin, which has preferably been produced from a monomer which is also the main monomer of the polyolefins of which foam layer A) consists. Accordingly, if layer A) consists of a foamed polypropylene and optionally a propylene-ethylene copolymer, layer C) may consist of polypropylene which optionally comprises grafted maleic anhydride units. Copolymers of ethylene-vinyl acetate may also be used as a further component. The thickness of layer C) is preferably 5 to 25 μm , particularly preferably 8 to 15 μm .

20

If the multilayer films according to the invention are to exhibit low gas permeability, i.e. low oxygen and moisture permeability together with aroma protection, they comprise a barrier layer E). This barrier layer is preferably composed of an ethylene-vinyl alcohol copolymer comprising a proportion of ethylene of 32 to 45 mol%, preferably of 35 to 42 mol%. The barrier layer E) may be bonded with the assistance of a coupling agent layer D) or F) on its respective surface with the bonding layer C) and with the heat-sealing layer G). The material used for this purpose is preferably a propylene copolymer or a polyethylene which comprises grafted maleic anhydride units.

30

The surface layer G), which forms the 2nd outer layer of the multilayer film according to the invention, is preferably heat-sealable and/or peelable. This layer is thus preferably produced using a low density polyethylene (LDPE) with a melt flow index (MFI) in the range from 0.5 to 8.0 g/10 min, preferably in the range from 1 to 5 g/10 min (2.16 kg, 190°C measured according to ASTM D1238) or an ionomer, such as for example a copolymer of an α -olefin and an ethylenically unsaturated carboxylic acid, wherein the carboxyl groups are present in an amount of 20 to 100 mol% as a metal salt, preferably as a sodium salt, or an ethylene-vinyl acetate copolymer with a vinyl acetate content of 3 to 10 wt.%, preferably of 4 to 6 wt.%, for the production of the heat-sealable layer.

According to a particularly preferred embodiment, the heat-sealing layer is also peelable. To this end, a blend of LDPE and a polybutylene (PB) is preferably used as the layer material. The blend preferably contains 15 to 30 wt.%, preferably 20 to 28 wt.%, of polybutylene. The polybutylene preferably has a melt flow index (MFI) in the range from 0.3 to 2.0 g/10 min (190°C and 2.16 kg according to ASTM 1238).

25

The thickness of the surface layer is preferably in the range from 10 to 50 μm , preferably from 15 to 30 μm .

If LDPE is used as the polymer for the production of the heat-sealing layer G) and the multilayer film according to the invention also comprises a barrier layer, a coupling agent layer is then preferably necessary for bonding the

- 8 -

barrier layer and the heat-sealing layer, unless an ethylene-vinyl alcohol copolymer is used as the barrier layer material. A polyolefin, preferably a polyethylene with grafted maleic anhydride units, may be used as the material for the coupling agent layer. It is, however, also possible to use a blend of LDPE and LLDPE in the ratio 3:1 to 4:1. The thickness of the particular coupling agent layer is in the range from 2 to 8 μm , preferably in the range from 3 to 6 μm .

10

The surface layer G) may contain conventional and known antibiotics, slip agents and antiblocking agents, such as for example erucamide, polyalkylsiloxanes, such as for example polydimethylsiloxane and/or silicon dioxide.

15

All or only individual layers of the multilayer film according to the invention may contain stabilisers and further additives of a known kind.

20 Layer B) may moreover contain 0.5 to 2 wt.% of a white pigment, such as for example kaolin, calcium carbonate, talcum, titanium dioxide or mixtures thereof. Such inorganic pigments are preferably added to the polymer, from which layer B) is produced, in the form of a masterbatch which contains 30 to 70 wt.% of pigments.

25

The multilayer films according to the invention may preferably be produced by conventional blown film coextrusion processes or by flat film coextrusion processes, inasmuch as this relates to the sequence of layers C) to G), and is preferably bonded with the polyolefin foam layer A) by an extrusion lamination step.

30

- 9 -

To this end, the foam layer A) and the multilayer film, consisting of layers C) to G), are brought together in such a manner that layer B) is extruded therebetween.

Immediately after extrusion, a sufficiently large pressure
5 is applied onto the resultant laminate to ensure that layers A) to G) are adequately bonded to one another.

It is, however, also possible to produce the multilayer films according to the invention solely by coextrusion,
10 wherein the foam layer A) is coextruded simultaneously with the other layers, optionally omitting layer C), and layer A) is simultaneously foamed.

The multilayer films according to the invention exhibit
15 excellent thermoformability on "FFS" machines (form-fill-seal machines) and may be converted on these machines into packaging containers, preferably into thermoformed packaging trays, then filled and sealed. It was surprising that the multilayer films according to the invention may
20 excellently be processed on FFS machines at an elevated production speed and, in comparison with a packaging material without the modification according to the invention, permit up to 10% shorter cycle times and thus an up to 10% higher output of packaging trays without any
25 impairment of the uniformity of wall thickness.

In comparison with comparable known, unmodified packaging materials, the multilayer films according to the invention also exhibit an unexpected improvement in mechanical
30 properties, in particular in rigidity measured by the modulus of elasticity in machine direction and in tensile stress. This distinct improvement is manifested without its

- 10 -

being necessary to increase the thickness of the multilayer films which are known from the prior art.

The packages produced from the multilayer films according
5 to the invention moreover exhibit distinctly more uniform surface structure, virtually without foam tears, so likewise improving the handling thereof.

The present invention accordingly also provides the use of
10 the multilayer film according to the invention as a packaging material, preferably on form-fill-seal machines (FFS machines), for packaging foodstuffs, in particular for packaging of highly perishable foodstuffs, such as meat, ham or sliced foodstuffs. Since packaging is often carried
15 out discontinuously on these machines, in order to package different products, the packaging material must also exhibit a relatively wide thermoforming "window" over which it may be thermoformed. This is the case for the packaging material according to the invention, as it exhibits
20 excellent thermoformability, in particular vacuum formability.

The thermoformed, preferably vacuum formed packaging articles, such as for example packaging trays, preferably
25 vacuum formed packaging trays, which have been produced from the multilayer films according to the invention, may, once filled, be sealed with known lidding films. Suitable lidding films are multilayer films, preferably made from polyethylene terephthalate/SiOx/coupling agent layer/low
30 density polyethylene or from polyethylene terephthalate/coupling agent layer/polyethylene/coupling

- 11 -

agent layer/ethylene-vinyl alcohol copolymer/coupling agent layer/polyethylene.

Among the stated lidding films, the first-stated multilayer
5 films are in particular suitable. To this end, the
biaxially oriented polyethylene terephthalate is coated
with SiO_x by plasma vacuum processing. The already
fabricated polyethylene film is then laminated thereto with
the assistance of a coupling agent. Such a lidding film is
10 in particular distinguished by excellent transparency and
elevated breaking strength. Packages comprising such a
lidding film moreover exhibit excellent gas barrier
properties.

15 In the following Examples, modulus of elasticity and
tensile stress are determined according to ISO 527-2 in
machine direction and in the transverse direction.

Examples:

Example 1

- 5 A multilayer film according to the invention with following layer structure:

Layer A) a foam layer with a density of 0.47 g/cm^3 and a cell count of 492 cells/mm^3 made from a blend of 50 wt.% polypropylene with long-chain branching (high melt strength polypropylene) and 46 wt.% of a heterophase propylene-ethylene block copolymer and 4 wt.% of finely divided talcum.

Layer B) made from 100 wt.% of a heterophase propylene-ethylene block copolymer corresponding to the block copolymer of foam layer A)

Layer C) made from a polypropylene,

Layer D) made from a coupling agent based on polypropylene grafted with maleic anhydride units,

Layer E) as a gas barrier layer based on an ethylene-vinyl alcohol copolymer,

Layer F) as a coupling agent layer with the same structure as layer D),

Layer G) as a heat-sealing layer based on low density polyethylene.

The multilayer film is produced by coextrusion. The
10 thickness of the individual layers is stated in Table 1.

Table 1

Layer	A)	B)	C)	D)	E)	F)	G)	Total
-------	----	----	----	----	----	----	----	-------

Thickness	1130	264	15	5	5	5	20	1444
in μm								

The mechanical properties of this film are stated in Table 2.

5 Comparative Example 1:

Corresponding to the multilayer film according to Example 1, a multilayer film was produced with an identical sequence of layers and, with the exception of layer A),
 10 with identical layer compositions and identical film thicknesses, wherein layer A) comprised the same polymer composition as in Example 1, but no nucleating agent.

The mechanical properties of the multilayer film according
 15 to the Comparative Example are stated in Table 2.

Table 2

	Unit	Comparative Example 1	Example 1
Modulus of elasticity (machine direction)	MPa	519	703
Modulus of elasticity (transverse direction)	MPa	280	280
Tensile stress (machine direction)	MPa	9.3	12.0
Tensile stress (transverse direction)	MPa	7.4	9.5
Cycle times	Cycles/minute	8	9

It is clear from Table 2 that the multilayer film according
 20 to the invention exhibits far better mechanical values than a multilayer film with an unmodified foam layer A).

IAP20 Rec'd PCT/PTO 25 APR 2006

EP-B-1 117 526 discloses complementing the foam layer with a compact layer of a polyolefin of the foam layer while maintaining a specific thickness ratio of these two layers to one another in order to improve the self-supporting properties of packages produced from this packaging material without increasing the thickness of the packaging material.

Although this packaging material may very readily be converted into packages, for example by thermoforming, there is a requirement due to ever higher packaging machinery running speeds to improve the packaging material in such a manner that it permits higher production speeds, i.e. shorter cycle times, without, for example, irregularities in the wall thickness of the packaging container consequently arising and without the mechanical strength or rigidity and thus the self-supporting properties of the packaging container being impaired.

Said object is achieved according to the invention by providing a multilayer film which comprises the following sequence of layers:

- A) a base layer of polyolefin foam containing 0.5 to 25 wt.%, relative to the total weight of the base layer, of at least one nucleating agent,
- B) a layer based on at least one polyolefin of the foam layer A),
- C) optionally a bonding layer based on a polyolefin, which is preferably based on the particular monomer

- 2 -

which is the main monomer of the polyolefin of foam layer A),

- D) optionally a coupling agent layer,
- E) optionally a gas- and/or aroma-barrier layer,
- 5 F) a coupling agent layer,
- G) an optionally heat-sealable and/or peelable surface layer,

wherein the total thickness of layers A) and B) is in the
10 range from 0.5 to 2 mm and the thickness of layer B) is in the range from $1/6$ to $1/2$ of the thickness of layer A).

Suitable nucleating agents are any known solid nucleating agents, preferably synthetic or natural inorganic
15 compounds. At least one nucleating agent selected from among the group comprising talcum, titanium dioxide, silicon dioxide, calcium carbonate, magnesium silicate, aluminium silicate, calcium phosphate and montmorillonite is particularly preferably used. Talcum is very
20 particularly preferably used.

The nucleating agent is added to the polymer from which the foam layer is to be produced, preferably in the form of a masterbatch which contains 30 to 60 wt.% of nucleating
25 agent in the polymer, and is largely homogeneously dispersed therein prior to foaming.

The foam layer A) obtained therefrom is distinguished by an elevated number of cells with relatively small size
30 deviations. The cell count is preferably greater than or equal to 250 cells/mm³, particularly preferably greater

than or equal to 300 cells/mm³ up to 600 cells/mm³, the size variations of the cells being in the range of $\pm 15\%$, preferably $\pm 10\%$. The density of the foam layer A) is preferably in the range from 0.35 to 0.55 g/cm³.

5

The density and cell count may moreover be varied by process parameters, such as for example extrusion temperature or other process parameters, during the preferred production of the foam layer by extrusion and
10 expansion.

Layer B) of compact polyolefin is substantially based on at least one polyolefin of the foamed base layer A). If this base layer consists of foamed polypropylene or a foamed
15 blend of polypropylene and propylene-ethylene copolymer, the compact polyolefin layer B) is preferably based on polypropylene or a propylene-ethylene copolymer. A heterophase propylene-ethylene block copolymer is particularly preferred. The melt flow index (MFI) of the
20 polyolefins used to produce layer B) is preferably in the range from 1.8 to 5.5 g/10 min measured as stated above. The thickness of layer B) amounts to $1/6$ to $1/2$, particularly preferably to $1/6$ to $1/3$ of the thickness of layer A).

25

Layer C) is preferably present, if layers D) to G) are prefabricated by coextrusion, preferably by blown film coextrusion, and are to be bonded with the other layers. Layer C) is based on a polyolefin, which has preferably
30 been produced from a monomer which is also the main monomer of the polyolefins of which foam layer A) consists.

Accordingly, if layer A) consists of a foamed polypropylene and optionally a propylene-ethylene copolymer, layer C) may consist of polypropylene which optionally comprises grafted maleic anhydride units. Copolymers of ethylene-vinyl acetate may also be used as a further component. The thickness of layer C) is preferably 5 to 25 μm , particularly preferably 8 to 15 μm .

If the multilayer films according to the invention are to exhibit low gas permeability, i.e. low oxygen and moisture permeability together with aroma protection, they comprise a barrier layer E). This barrier layer is preferably composed of an ethylene-vinyl alcohol copolymer comprising a proportion of ethylene of 32 to 45 mol%, preferably of 35 to 42 mol%. The barrier layer E) may be bonded with the assistance of a coupling agent layer D) or F) on its respective surface with the bonding layer C) and with the heat-sealing layer G). The material used for this purpose is preferably a propylene copolymer or a polyethylene which comprises grafted maleic anhydride units.

The surface layer G), which forms the 2nd outer layer of the multilayer film according to the invention, is preferably heat-sealable and/or peelable. This layer is thus preferably produced using a low density polyethylene (LDPE) with a melt flow index (MFI) in the range from 0.5 to 8.0 g/10 min, preferably in the range from 1 to 5 g/10 min (2.16 kg, 190°C measured according to ASTM D1238) or an ionomer, such as for example a copolymer of an α -olefin and an ethylenically unsaturated carboxylic acid, wherein the carboxyl groups are present in an amount of 20 to 100 mol%

as a metal salt, preferably as a sodium salt, or an ethylene-vinyl acetate copolymer with a vinyl acetate content of 3 to 10 wt.%, preferably of 4 to 6 wt.%, for the production of the heat-sealable layer.

5

According to a particularly preferred embodiment, the heat-sealing layer is also peelable. To this end, a blend of LDPE and a polybutylene (PB) is preferably used as the layer material. The blend preferably contains 15 to 30
10 wt.%, preferably 20 to 28 wt.%, of polybutylene. The polybutylene preferably has a melt flow index (MFI) in the range from 0.3 to 2.0 g/10 min (190°C and 2.16 kg according to ASTM 1238).

15 The thickness of the surface layer is preferably in the range from 10 to 50 µm, preferably from 15 to 30 µm.

If LDPE is used as the polymer for the production of the heat-sealing layer G) and the multilayer film according to
20 the invention also comprises a barrier layer, a coupling agent layer is then preferably necessary for bonding the barrier layer and the heat-sealing layer, unless an ethylene-vinyl alcohol copolymer is used as the barrier layer material. A polyolefin, preferably a polyethylene
25 with grafted maleic anhydride units, may be used as the material for the coupling agent layer. It is, however, also possible to use a blend of LDPE and LLDPE in the ratio 3:1 to 4:1. The thickness of the particular coupling agent layer is in the range from 2 to 8 µm, preferably in the
30 range from 3 to 6 µm.

The surface layer G) may contain conventional and known antibiotics, slip agents and antiblocking agents, such as for example erucamide, polyalkylsiloxanes, such as for example polydimethylsiloxane and/or silicon dioxide.

5

All or only individual layers of the multilayer film according to the invention may contain stabilisers and further additives of a known kind.

- 10 Layer B) may moreover contain 0.5 to 2 wt.% of a white pigment, such as for example kaolin, calcium carbonate, talcum, titanium dioxide or mixtures thereof. Such inorganic pigments are preferably added to the polymer, from which layer B) is produced, in the form of a
- 15 masterbatch which contains 30 to 70 wt.% of pigments.

The multilayer films according to the invention may preferably be produced by conventional blown film coextrusion processes or by flat film coextrusion

20 processes, inasmuch as this relates to the sequence of layers C) to G), and is preferably bonded with the polyolefin foam layer A) by an extrusion lamination step. To this end, the foam layer A) and the multilayer film, consisting of layers C) to G), are brought together in such

25 a manner that layer B) is extruded therebetween.

Immediately after extrusion, a sufficiently large pressure is applied onto the resultant laminate to ensure that layers A) to G) are adequately bonded to one another.

- 30 It is, however, also possible to produce the multilayer films according to the invention solely by coextrusion,

wherein the foam layer A) is coextruded simultaneously with the other layers, optionally omitting layer C), and layer A) is simultaneously foamed.

5 The multilayer films according to the invention exhibit excellent thermoformability on "FFS" machines (form-fill-seal machines) and may be converted on these machines into packaging containers, preferably into thermoformed packaging trays, then filled and sealed. It was surprising
10 that the multilayer films according to the invention may excellently be processed on FFS machines at an elevated production speed and, in comparison with a packaging material without the modification according to the invention, permit up to 10% shorter cycle times and thus an
15 up to 10% higher output of packaging trays without any impairment of the uniformity of wall thickness.

In comparison with comparable known, unmodified packaging materials, the multilayer films according to the invention
20 also exhibit an unexpected improvement in mechanical properties, in particular in rigidity measured by the modulus of elasticity in machine direction and in tensile stress. This distinct improvement is manifested without its being necessary to increase the thickness of the multilayer
25 films which are known from the prior art.